

## Where we are:

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## Important concepts, symbols, and equations

For a single joint with the joint velocity as the control:

- **Open-loop (feedforward) control:**  $\dot{\theta}(t) = \dot{\theta}_d(t)$
- **Closed-loop (feedback) control:**  $\dot{\theta}(t) = f(\theta_d(t), \theta(t))$
- **FF + Proportional-Integral (PI) FB control:**

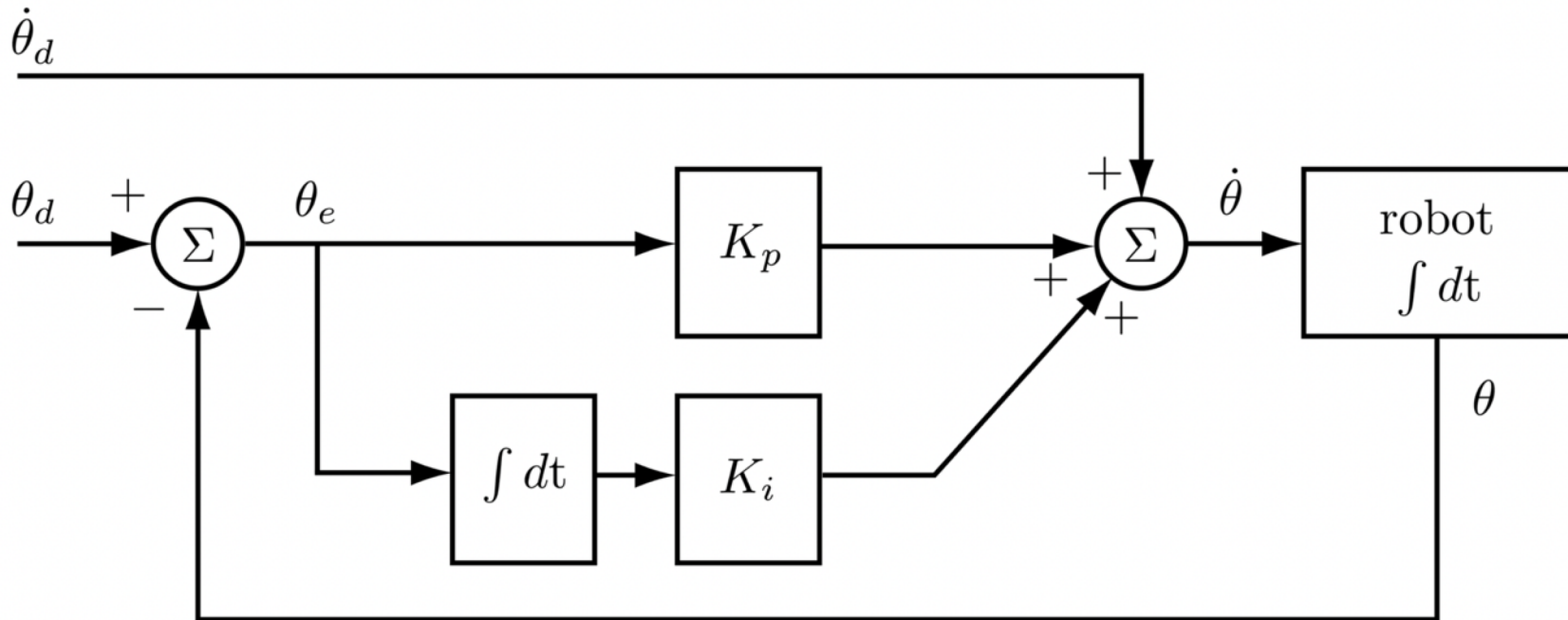
$$\dot{\theta}(t) = \dot{\theta}_d(t) + K_p \theta_e(t) + K_i \int_0^t \theta_e(t) dt, \quad K_p, K_i \geq 0$$

- *reduces to FF control if  $K_p, K_i = 0$*
- *if no FF term: **P control** when  $K_i = 0$ , **I control** when  $K_p = 0$*

What is the point of FF control in this control law?

## Important concepts, symbols, and equations (cont.)

Block diagram



$$\dot{\theta}(t) = \dot{\theta}_d(t) + K_p \theta_e(t) + K_i \int_0^t \theta_e(t) dt$$

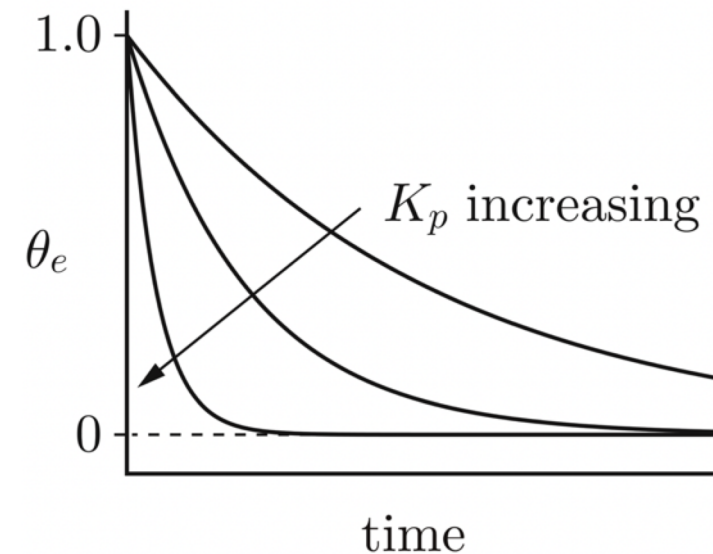
## Important concepts, symbols, and equations (cont.)

**Setpoint control**,  $\theta_d(t) = c$ , with a P controller

$$\dot{\theta}_e(t) = \dot{\theta}_d(t) - \dot{\theta}(t)$$

$$\dot{\theta}_e(t) = -K_p \theta_e(t) \rightarrow \dot{\theta}_e(t) + K_p \theta_e(t) = 0$$
$$\tau = 1/K_p$$

$$\theta_e(t) = e^{-t/\tau} \theta_e(0)$$





## Important concepts, symbols, and equations (cont.)

Constant velocity control,  $\theta_d(t) = ct + a$

P control

$$\dot{\theta}_e(t) = \dot{\theta}_d(t) - \dot{\theta}(t) = c - K_p\theta_e(t)$$

$$\dot{\theta}_e(t) + K_p\theta_e(t) = c$$

$$\theta_e(t) = \frac{c}{K_p} + \left( \theta_e(0) - \frac{c}{K_p} \right) e^{-K_p t}$$

PI control

$$\dot{\theta}(t) = K_p\theta_e(t) + K_i \int_0^t \theta_e(t) dt$$

$$\dot{\theta}_e(t) + K_p\theta_e(t) + K_i \int_0^t \theta_e(t) dt = c$$

$$\ddot{\theta}_e(t) + K_p\dot{\theta}_e(t) + K_i\theta_e(t) = 0$$

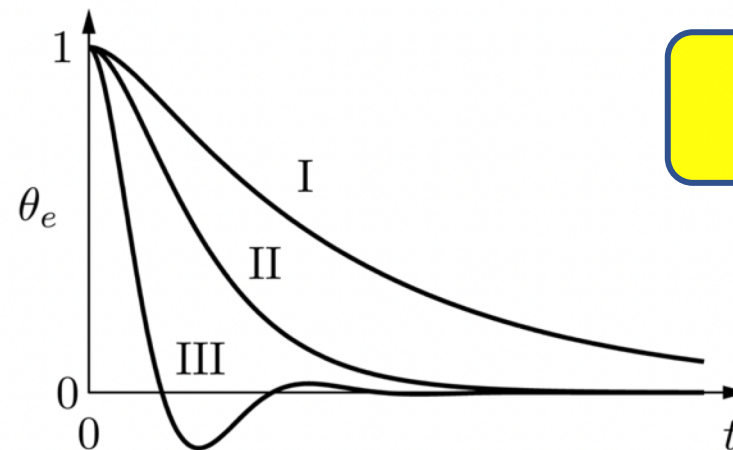
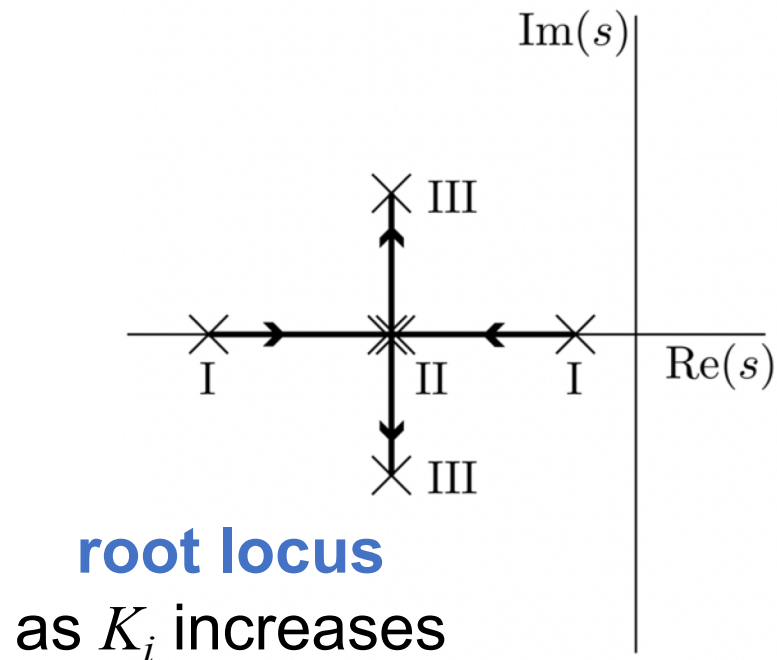
$$\zeta = K_p / (2\sqrt{K_i})$$

$$\omega_n = \sqrt{K_i}$$

## Important concepts, symbols, and equations (cont.)

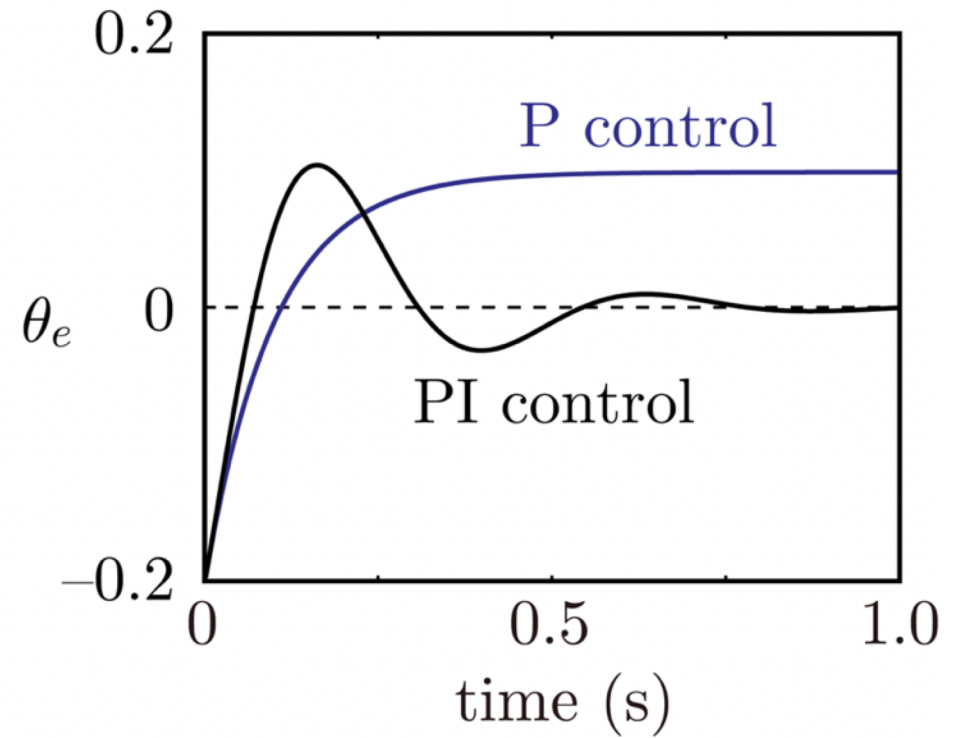
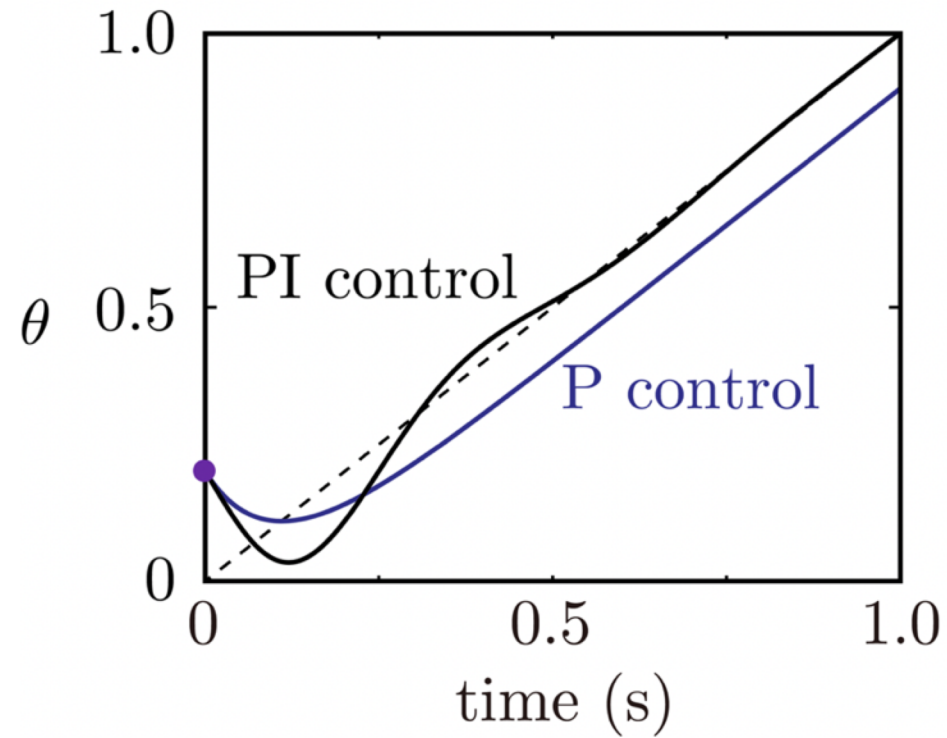
characteristic equation of PI error dynamics:  $s^2 + K_p s + K_i = 0$

$$s_{1,2} = -\frac{K_p}{2} \pm \sqrt{\frac{K_p^2}{4} - K_i}$$



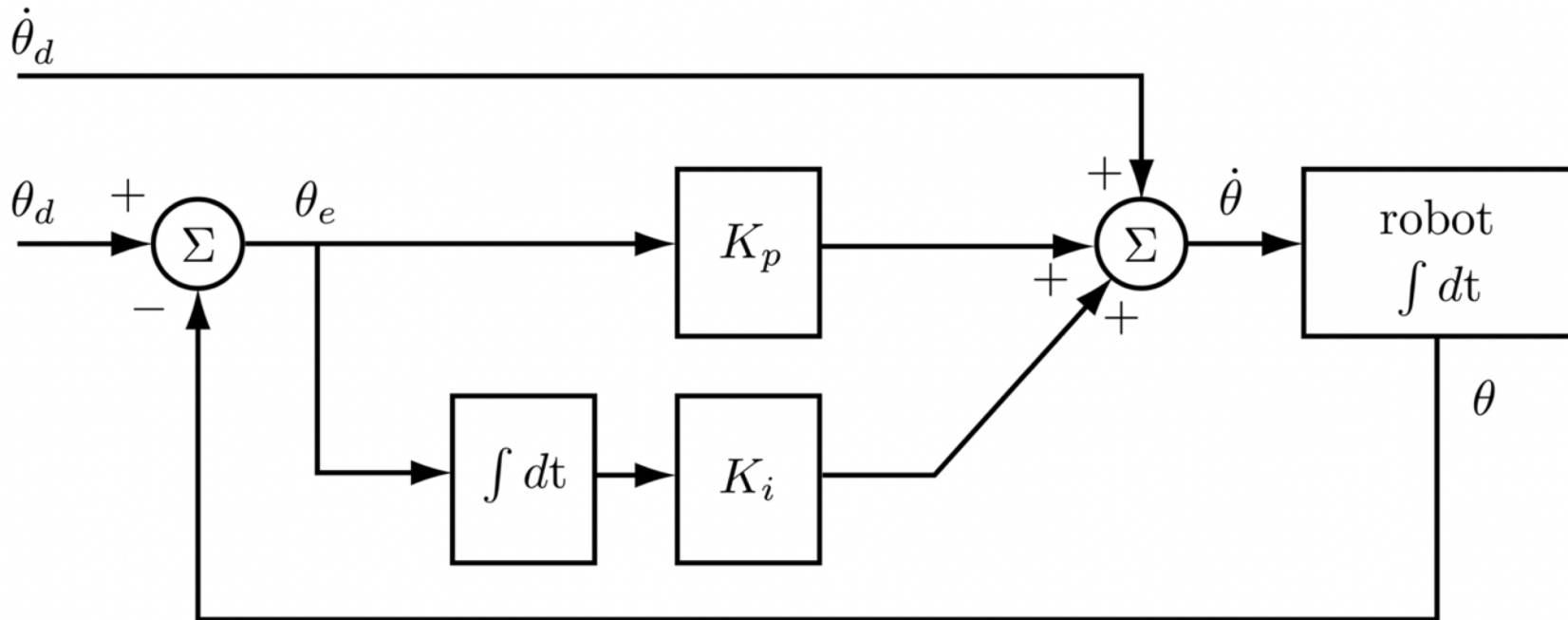
What if  $K_i = 0$ ?

## Important concepts, symbols, and equations (cont.)



## Important concepts, symbols, and equations (cont.)

**Multi-joint control:**  $\theta$ ,  $\theta_d$ , and  $\theta_e$  are vectors and  $K_p = k_p I$ ,  $K_i = k_i I$



$$\dot{\theta}(t) = \dot{\theta}_d(t) + K_p \theta_e(t) + K_i \int_0^t \theta_e(t) dt$$

## Important concepts, symbols, and equations (cont.)

$$\dot{\theta}(t) = \dot{\theta}_d(t) + K_p \theta_e(t) + K_i \int_0^t \theta_e(t) dt$$

### Task-space motion control

desired motion  $X_d \in SE(3)$

$$[\mathcal{V}_d] = X_d^{-1} \dot{X}_d$$

actual motion  $X \in SE(3)$

$$[\mathcal{V}_b] = X^{-1} \dot{X}$$

error:  $[X_e] = \log X_{bd} = \log(X^{-1} X_d)$

$$\mathcal{V}_b(t) = [\text{Ad}_{X_{bd}}] \mathcal{V}_d(t) + K_p X_e(t) + K_i \int_0^t X_e(t) dt$$
$$\dot{\theta} = J_b^\dagger(\theta) \mathcal{V}_b$$



## Important concepts, symbols, and equations (cont.)

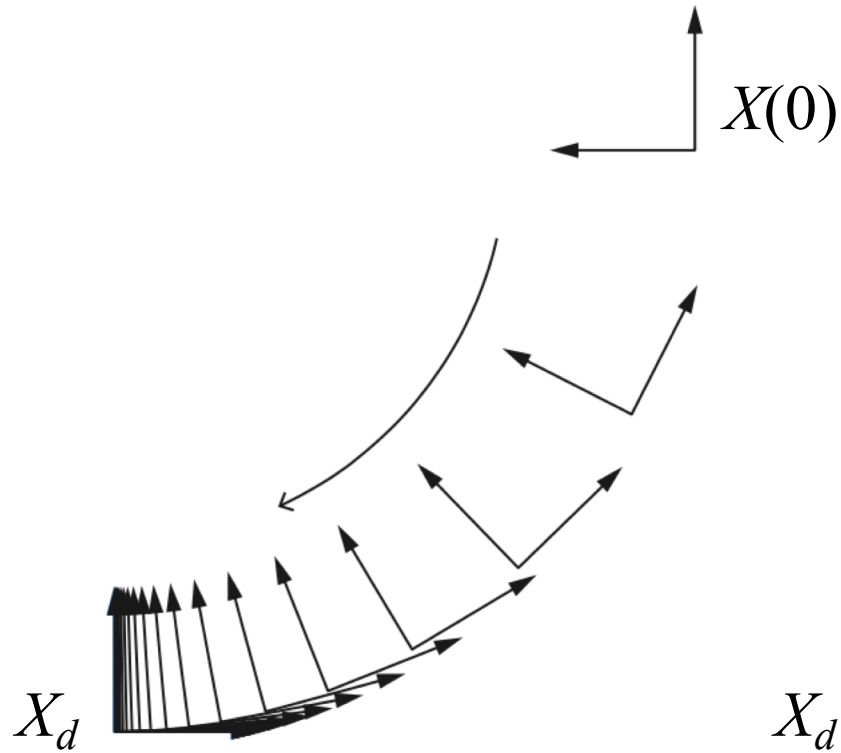
### Decoupled task-space motion control

$$X_e(t) = \begin{bmatrix} \omega_e(t) \\ p_d(t) - p(t) \end{bmatrix} \quad [\omega_e] = \log(R^T R_d)$$

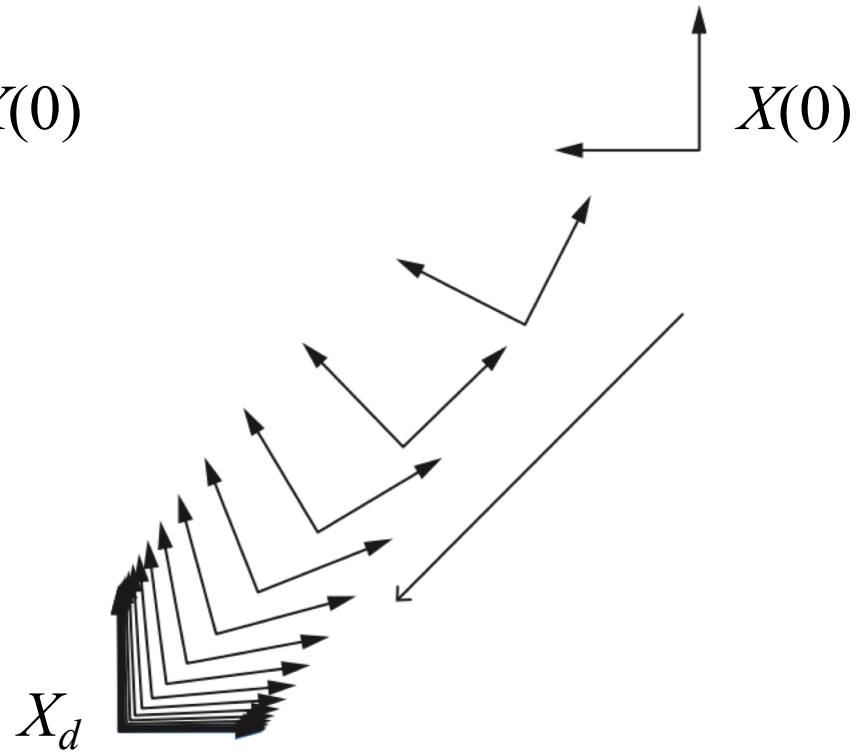
$$\begin{bmatrix} \omega_b(t) \\ \dot{p}(t) \end{bmatrix} = \begin{bmatrix} R^T(t)R_d(t) & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} \omega_d(t) \\ \dot{p}_d(t) \end{bmatrix} + K_p X_e(t) + K_i \int_0^t X_e(t) dt$$
$$\dot{\theta} = J^\dagger(\theta) \begin{bmatrix} \omega_b(t) \\ \dot{p}(t) \end{bmatrix}$$

What is this Jacobian?

## Important concepts, symbols, and equations (cont.)



task-space P controller



decoupled task-space P controller



You are designing a P controller to track a joint reference trajectory that is moving at a constant rate of 3 radians/s. What is the smallest gain  $K_p$  that ensures a steady-state position error of no more than 0.1 radians? Give units.

To eliminate steady-state error, you decide to use a PI controller. What gains  $K_p$  and  $K_i$  should you choose to achieve critical damping and a settling time of 0.1 s? Give units.

Explain how to estimate the error integral if the controller's frequency is  $1/T$ .

Why not choose arbitrarily large  $K_p$  and  $K_i$  to achieve arbitrarily fast settling?

How well would a PI controller track a quadratic joint trajectory? (Not a ramp.)