

# Time-optimal time scaling

## Chapter 9

Introduction to Robotics:  
Mechanics, Planning, and Control  
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# Time-optimal time scaling of a path

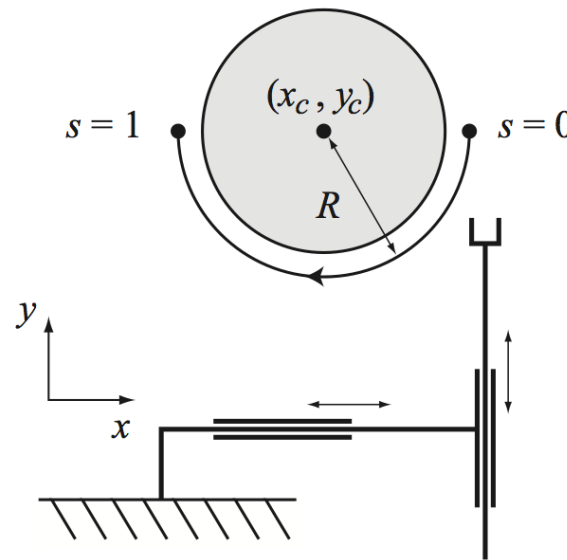


Figure 9.8: A path planner has returned a semicircular path of radius  $R$  around an obstacle in  $(x, y)$  space for a robot with two prismatic joints. The path can be represented as a function of a path parameter  $s$  as  $x(s) = x_c + R \cos s\pi$  and  $y(s) = y_c - R \sin s\pi$  for  $s \in [0, 1]$ . For a 2R robot, inverse kinematics would be used to express the path as a function of  $s$  in joint coordinates.

# Dynamics constrained to a path

$$M(\theta)\ddot{\theta} + C(\theta, \dot{\theta})\dot{\theta} + g(\theta) = \tau,$$

$$C(\theta, \dot{\theta})\dot{\theta} = \dot{\theta}^T \Gamma(\theta) \dot{\theta}$$

replacing  $\dot{\theta}$  by  $(d\theta/ds)\dot{s}$

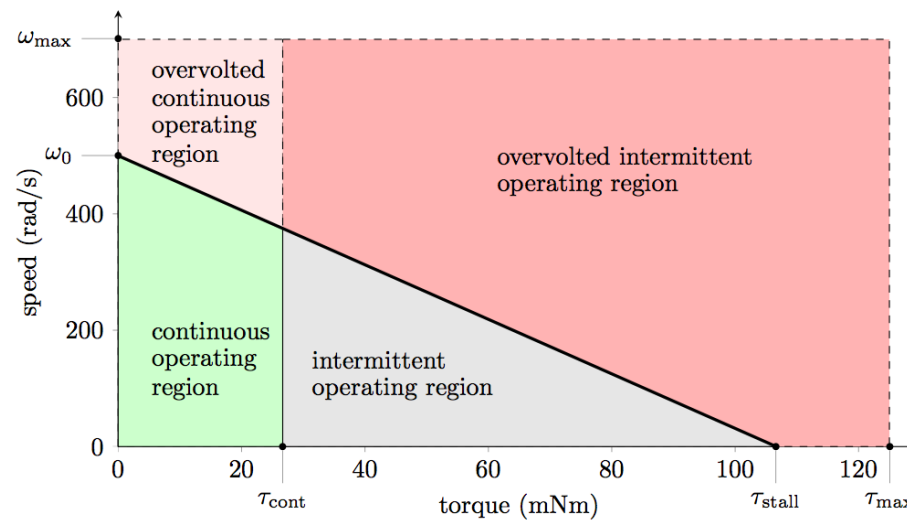
and  $\ddot{\theta}$  by  $(d\theta/ds)\ddot{s} + (d^2\theta/ds^2)\dot{s}^2$ .

$$\underbrace{\left( M(\theta(s)) \frac{d\theta}{ds} \right)}_{m(s)} \ddot{s} + \underbrace{\left( M(\theta(s)) \frac{d^2\theta}{ds^2} + \left( \frac{d\theta}{ds} \right)^T \Gamma(\theta(s)) \frac{d\theta}{ds} \right)}_{c(s)} \dot{s}^2 + \underbrace{g(\theta(s))}_{g(s)} = \tau.$$

$$m(s)\ddot{s} + c(s)\dot{s}^2 + g(s) = \tau,$$

# Actuator torque/force limits

$$\tau_i^{\min}(\theta, \dot{\theta}) \leq \tau_i \leq \tau_i^{\max}(\theta, \dot{\theta})$$



$$\tau_i^{\min}(s, \dot{s}) \leq m_i(s)\ddot{s} + c_i(s)\dot{s}^2 + g_i(s) \leq \tau_i^{\max}(s, \dot{s})$$

# Acceleration limits

$$\tau_i^{\min}(s, \dot{s}) \leq m_i(s)\ddot{s} + c_i(s)\dot{s}^2 + g_i(s) \leq \tau_i^{\max}(s, \dot{s})$$

$$\text{if } m_i(s) > 0 : \quad L_i(s) = \frac{\tau_i^{\min}(s, \dot{s}) - c_i(s)\dot{s}^2 - g_i(s)}{m_i(s)}$$

$$U_i(s) = \frac{\tau_i^{\max}(s, \dot{s}) - c_i(s)\dot{s}^2 - g_i(s)}{m_i(s)}$$

$$\text{if } m_i(s) < 0 : \quad L_i(s) = \frac{\tau_i^{\max}(s, \dot{s}) - c_i(s)\dot{s}^2 - g_i(s)}{m_i(s)}$$

$$U_i(s) = \frac{\tau_i^{\min}(s, \dot{s}) - c_i(s)\dot{s}^2 - g_i(s)}{m_i(s)}$$

if  $m_i(s) = 0$  : *zero-inertia point*, discussed in Section 9.4.3

# The problem statement

$$L(s, \dot{s}) = \max_i L_i(s, \dot{s}) \quad \text{and} \quad U(s, \dot{s}) = \min_i U_i(s, \dot{s}).$$
$$L(s, \dot{s}) \leq \ddot{s} \leq U(s, \dot{s}).$$

*Given a path  $\theta(s)$ ,  $s \in [0, 1]$ , an initial state  $(s_0, \dot{s}_0) = (0, 0)$ , and a final state  $(s_f, \dot{s}_f) = (1, 0)$ , find a monotonically increasing twice-differentiable time scaling  $s : [0, T] \rightarrow [0, 1]$  that*

- (i) satisfies  $s(0) = \dot{s}(0) = \dot{s}(T) = 0$  and  $s(T) = 1$ , and*
- (ii) minimizes the total travel time  $T$  along the path while respecting the actuator constraints (9.37).*

# The $(s, \dot{s})$ phase plane

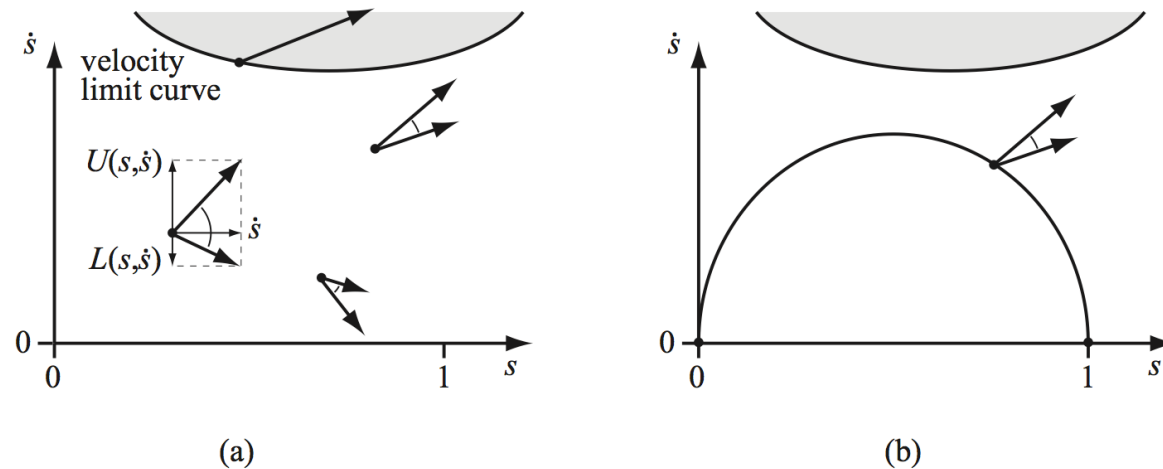
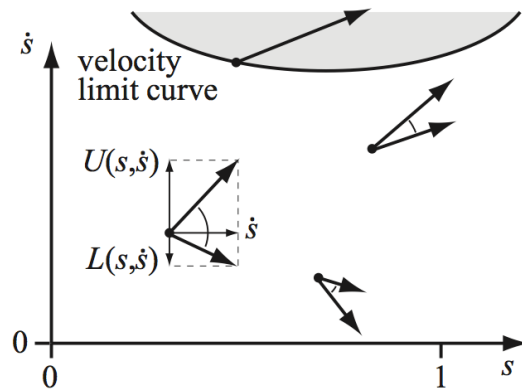


Figure 9.10: (a) Acceleration-limited motion cones at four different states. The upper ray of the cone is the sum of  $U(s, \dot{s})$  plotted in the vertical direction (change in velocity) and  $\dot{s}$  plotted in the horizontal direction (change in position). The lower ray of the cone is constructed from  $L(s, \dot{s})$  and  $\dot{s}$ . Points in grey, bounded by the velocity limit curve, have  $L(s, \dot{s}) \geq U(s, \dot{s})$ —the state is inadmissible. On the velocity limit curve, the cone is reduced to a single tangent vector. (b) The proposed time scaling is infeasible because the tangent to the curve is outside the motion cone at the state indicated.

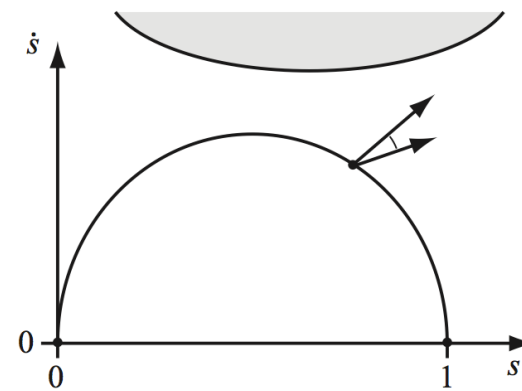
Maximize “speed”  $\dot{s}$  at all  $s$  while satisfying acceleration and boundary constraints

$$T = \int_0^T 1 \, dt.$$

$$T = \int_0^t 1 \, dt = \int_0^T \frac{ds}{\dot{s}} \, dt = \int_0^T \frac{dt}{\dot{s}} \, ds = \int_0^1 \dot{s}^{-1}(s) \, ds$$



(a)



(b)



# Time-optimal “bang-bang” time scaling

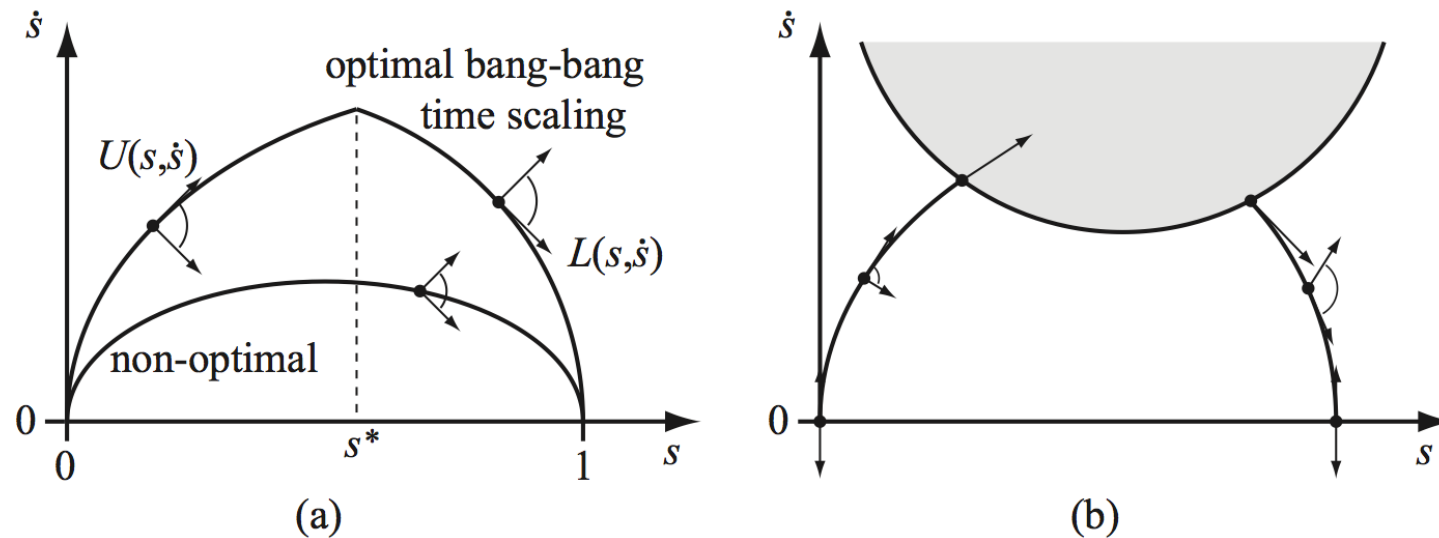
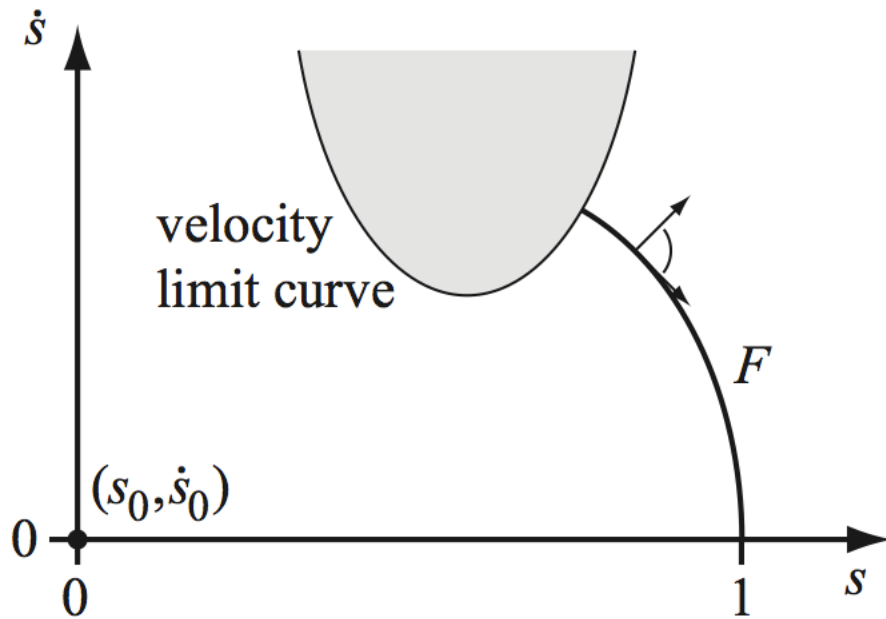


Figure 9.11: (a) A time-optimal bang-bang time scaling integrates  $U(s, \dot{s})$  from  $(0,0)$  and switches to  $L(s, \dot{s})$  at a switching point  $s^*$ . Also shown is a non-optimal time scaling with a tangent inside a motion cone. (b) Sometimes the velocity limit curve prevents a single-switch solution.

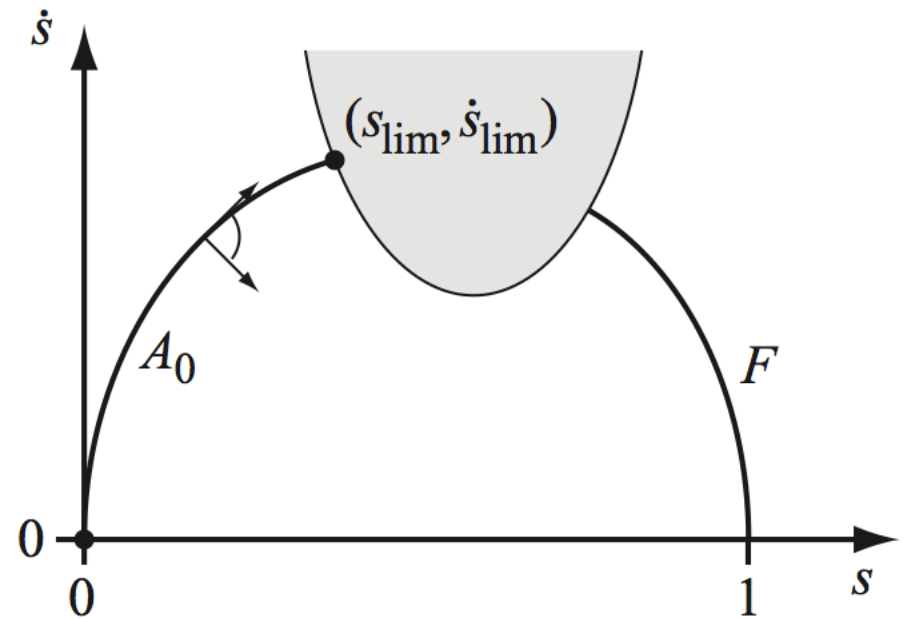
# Time-scaling algorithm

1. Initialize empty list of switches  $S$  between  $U$  and  $L$ .
2. Integrate backward from end along  $L$ .
3. Integrate forward from start along  $U$ . If the curve crosses the final curve, switch  $U$  to  $L$  occurs there. Done.
4. If speed limit is exceeded, lower the speed at the penetration  $s$  until velocity limit not reached when integrating forward along  $U$ . Call the point just touching the speed limit  $B$ .
5. Integrate backward along  $L$  from  $B$  until intersecting the previous  $U$  motion segment. Switch to  $L$  occurs there.
6. Switch to  $U$  occurs at  $B$ . Set “start” to  $B$ , go to step 3.

## Steps 2 and 3

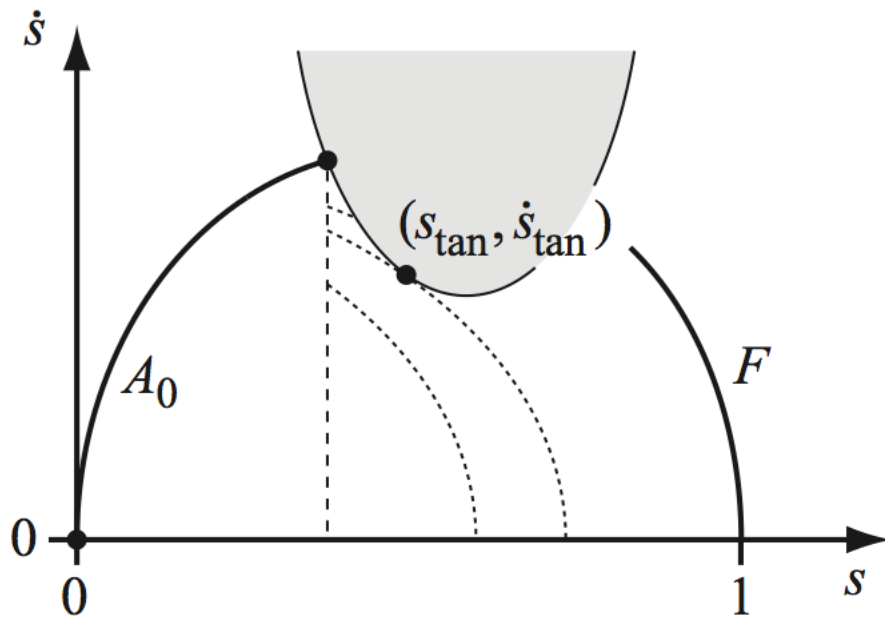


Step 2:  $i = 0, S = \{\}$

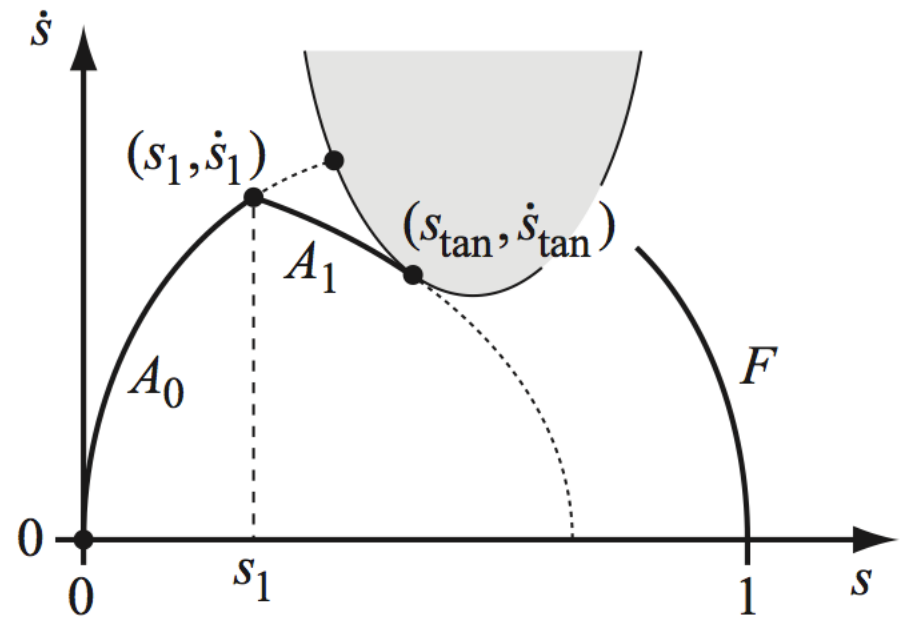


Step 3:  $i = 0, S = \{\}$

## Steps 4 and 5

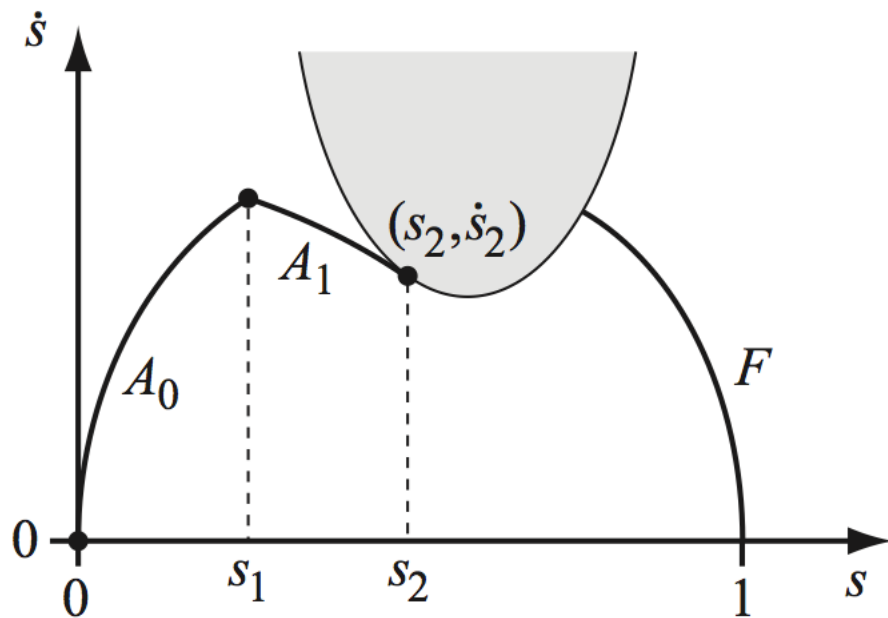


Step 4:  $i = 0, S = \{\}$

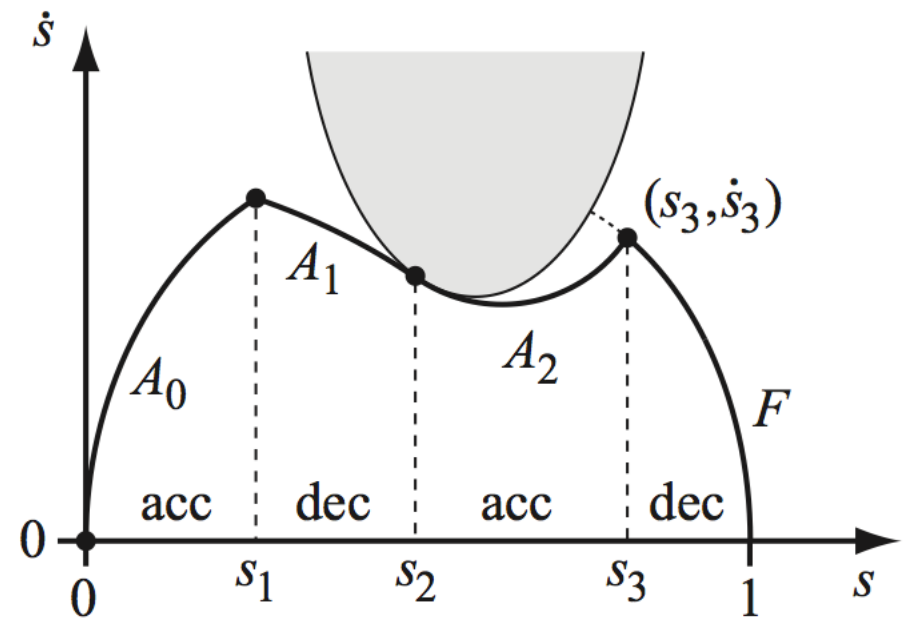


Step 5:  $i = 1, S = \{s_1\}$

## Step 6, and back to step 3



Step 6:  $i = 2$ ,  $S = \{s_1, s_2\}$



Step 3:  $i = 3$ ,  $S = \{s_1, s_2, s_3\}$

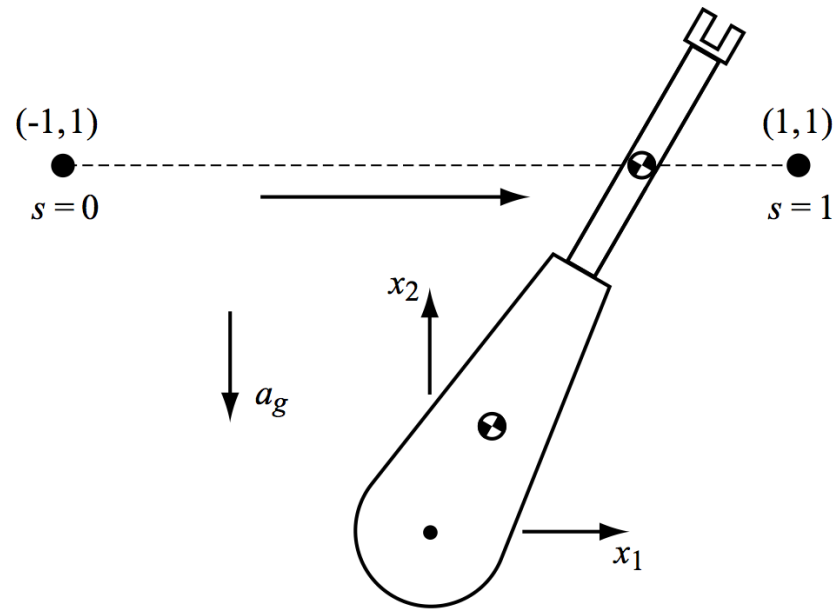
# Assumptions

- Actuators are strong enough to hold static posture at all  $s$
- Single speed limit for all  $s$
- No zero-inertia points (zip) where one or more  $m_i = 0$   
if isolated zips, or a “singular arc” of zips, then some actuator speed constraints come directly from

$$\tau_i^{\min}(s, \dot{s}) \leq \cancel{m_i(s)} \overset{0}{\ddot{s}} + c_i(s) \dot{s}^2 + g_i(s) \leq \tau_i^{\max}(s, \dot{s})$$

and others from  $L_i(s, \dot{s}) = U_i(s, \dot{s})$

# Zero-inertia point



for actuator 2 at  $s = 1/2$